

DESCRIPTION

SEAMLESS EXPANDABLE OIL COUNTRY TUBULAR GOODS AND
MANUFACTURING METHOD THEREOF

Technical Field

[0001] The present invention relates to seamless expandable oil country tubular goods used in oil wells or gas wells (hereinafter collectively referred to as "oil wells") and manufacturing methods thereof. The present invention relates to seamless expandable oil country tubular goods that can be expanded in a well and can be used as a casing or a tubing without any additional treatment. In more particular, the present invention relates to the seamless expandable oil country tubular goods having a tensile strength of 600 MPa or more and a yield ratio of 85% or less and a manufacturing method thereof. The steel pipes used in oil wells are called "oil country tubular goods".

Background Art

[0002] In recent years, due to the requirement of reduction in cost for drilling of oil wells, construction methods have been developed in which pipe expansion is performed in a well using a expanding process (for example, see The Patent Documents 1 and 2). Hereinafter, this construction method is called a solid expandable tubular system. According to this solid expandable tubular system, a casing is expanded radially in a well. Compared to a conventional construction method, when the same well radius is to be ensured, each of the diameters of individual sections forming a casing having a multistage structure can be decreased. In addition, since the size of a casing for an exterior layer of an upper portion of the well can also be decreased, the cost for drilling a well can be reduced.

[0003] In the solid expandable tubular system described above, since being exposed to oil or gas environment immediately after a expanding process is carried out, steel pipes thus formed are not processed by heat treatment after the process described above, and hence the steel pipes are required to have corrosion resistance as cold expanded. In order to satisfy the requirement described above, The Patent Document 3 discloses expandable oil country tubular goods having superior corrosion resistance after a expanding process. The Patent Document 3 discloses the expandable oil country tubular goods comprising 0.10% to 0.45% of C, 0.1% to 1.5% of Si, 0.10% to 3.0% of Mn, 0.03% or less of P, 0.01% or less of S, 0.05% or less of sol. Al, and 0.010% or less of N are contained on a mass percent basis, the balance being composed of Fe and impurities. The Patent Document 3 discloses a steel pipe, in which the strength (yield strength YS (MPa)) before a expanding process and the crystal grain diameter ($d(\mu\text{m})$) satisfy an equation represented by $\ln(d) \leq -0.0067YS + 8.09$. In addition, it has also been disclosed that, in the same steel pipe described above, (A) at least one of 0.2% to 1.5% of Cr, 0.1% to 0.8% of Mo, and 0.005% to 0.2% of V on a mass percent basis, (B) at least one of 0.005% to 0.05% of Ti and 0.005% to 0.03% of Nb on a mass percent basis, and (C) at least one of 0.001% to 0.005% of Ca are contained instead of a part of the Fe.

[0004] In addition, The Patent Document 4 has disclosed that, in order to prevent the decrease in collapse strength caused by the increase in rate of wall-thickness deviation by pipe expansion, the rate of wall-thickness deviation EO (%) before pipe expansion is controlled to be $30/(1+0.018\alpha)$ or less (where α (expand ratio) = (inside diameter after pipe expansion/inside diameter before pipe expansion-1)×100), and that in addition, in order to prevent a steel pipe from being bent which is caused by the conversion of the difference in expansion amount in the circumferential direction to the difference in contraction amount in the longitudinal direction, the

rate of eccentric wall-thickness deviation (primary wall-thickness deviation) (%) (= {(maximum wall thickness of a component of eccentric wall-thickness deviation - minimum wall thickness thereof)/average wall thickness}×100) is controlled to be 10% or less.

[0005] According to Patent Documents 3 and 4, a preferable manufacturing method has been disclosed in which quenching and tempering are performed for electric resistance welded steel pipes or seamless steel pipes obtained after pipe forming or in which quenching is repeatedly performed therefor at least two times, followed by tempering, and an example has been disclosed in which a expanding process is performed within an expand ratio of 30% or less.

Patent Document 1: PCT Japanese Translation Patent Publication No. 7-567610

Patent Document 2: International Patent Application Publication No. WO98/00626

Patent Document 3: Japanese Unexamined Patent Application Publication No. 2002-266055

Patent Document 4: Japanese Unexamined Patent Application Publication No. 2002-349177

Disclosure of Invention

[0006] However, due to further requirement of cost reduction, inexpensive steel pipes has been desired which can withstand an expanding process performed at a high expand ratio, such as more than 30%. When a steel pipe can be expanded in a well at an expand ratio larger than a conventional value of 30%, the size of casing can be further decreased, and hence drilling cost can be further decreased. In order to satisfy the requirement described above, an object of the present invention is to provide a seamless expandable oil country tubular goods, which has an excellent pipe-expansion property capable of withstanding a expanding process at an expand ratio of more than 30% although having a high strength, such as a tensile strength (TS) of 600 MPa or more, and a manufacturing method thereof. In addition, unlike the case disclosed in The

unexamined patent publication bulletins 3 and 4, without receiving quenching and tempering (Q/T) treatment, the seamless expandable oil country tubular goods described above is in an as-rolled state or is processed by nonthermal-refining type heat treatment (normalizing (annealing) treatment or dual-phase heat treatment) which is more inexpensive heat treatment.

[0007] The pipe-expansion property described above is to be evaluated by a limit of expand ratio at which expansion can be performed without causing any non-uniform deformation of a pipe when it is expanded, and in the present invention, in particular, an expand ratio at which the rate of wall-thickness deviation after expansion is not more than the rate of wall-thickness deviation before expansion + 5% is used.

Expand Ratio (%) = [(inside diameter of pipe after pipe expansion - inside diameter of pipe before pipe expansion)/inside diameter of pipe before pipe expansion] × 100

Rate of Wall-Thickness Deviation = [(maximum wall thickness of pipe - minimum wall thickness of pipe)/average wall thickness of pipe] × 100

[0008] Major properties required for an expandable steel pipe are that pipe expansion can be easily performed, that is, can be performed using small energy, and that in pipe expansion even at a high expand ratio, a steel pipe is not likely to be unevenly deformed so that uniform deformation is obtained. For performing easy pipe expansion, a low YR (YR: yield ratio = yield strength YS/tensile strength TS) is preferable, and in addition, for obtaining uniform deformation even at a high expand ratio, a high uniform elongation and a high work-hardening coefficient are preferable.

[0009] In order to achieve the properties described above, the inventors of the present invention found that a preferable microstructure of a steel pipe substantially contains ferrite (volume fraction of 5% or more) + a low temperature-transforming phase (bainite, martensite, bainitic

ferrite, or a mixture containing at least two thereof), and hence various researches were carried out to realize the microstructure described above.

[0010] First, the content of C was controlled to be less than 0.1% for suppressing the formation of perlite and for increasing the toughness, Nb was further added which was an element having an effect of delaying transformation, and subsequently, the content of Mn forming a microstructure containing ferrite and a low temperature-transforming phase was examined. In this case, the formation of a predetermined microstructure by cooling a pipe from a γ region was defined as the essential condition, and by the use of a steel pipe having an external diameter of 4" to $9\frac{5}{8}$ " and a wall thickness of 5 to 12 mm, which has been currently considered to be applied to an expandable steel pipe, as the standard pipe, it was intended to obtain a predetermined microstructure by a cooling rate which is generally applied to the size of the steel pipe described above. Although depending on circumstances in cooling, the average cooling rate is approximately 0.2 to 2°C/sec in the range of approximately 700 to 400°C.

[0011] As a result, it was found that when the content of Mn is 2% to 4%, ferrite is formed and a low temperature-transforming phase is formed without forming perlite. In addition, it was also found that when a predetermined amount of Mo or Cr, which is also an element having an effect of delaying transformation, is added instead of Nb, the same effect as described above is obtained.

[0012] Through further intensive researches carried out by the inventors of the present invention, it was disclosed that when the content of Mn is controlled to be 0.5% or more, and an alloying element is added so that equation (1) or (3) holds, the formation of perlite is suppressed. In addition, it was also disclosed that since a ferrite microstructure is no longer formed when a large amount of an alloying element is added, the addition thereof must be performed so as to

satisfy equation (2) or (4) for forming a ferrite microstructure. That is, by satisfying both equations, a microstructure containing ferrite and a low temperature-transforming phase can be formed, and hence a steel pipe having a high expand ratio and a low YR can be obtained.

$$\text{Mn}+0.9\times\text{Cr}+2.6\times\text{Mo}\geq 2.0 \quad (1)$$

$$4\times\text{C}-0.3\times\text{Si}+\text{Mn}+1.3\times\text{Cr}+1.5\times\text{Mo}\leq 4.5 \quad (2)$$

$$\text{Mn}+0.9\times\text{Cr}+2.6\times\text{Mo}+0.3\times\text{Ni}+0.3\times\text{Cu}\geq 2.0 \quad (3)$$

$$4\times\text{C}-0.3\times\text{Si}+\text{Mn}+1.3\times\text{Cr}+1.5\times\text{Mo}+0.3\times\text{Ni}+0.6\times\text{Cu}\leq 4.5 \quad (4)$$

In the above equations, the symbol of element represents the content (mass percent) of the element contained in steel.

[0013] From steel developed based on the above findings, a predetermined microstructure containing ferrite and low temperature-transforming phase can be obtained by air cooling performed from the γ region, and in addition, it was also found that when this steel is held in an (α/γ) dual-phase region, followed by air cooling, the YR can be further decreased.

[0014] The reason the pipe-expansion property is improved by the formation of a dual-phase microstructure has not been understood in detail; however, it has been considered that by the formation of a dual-phase microstructure, the work-hardening coefficient is increased, a thin wall portion first has a deformation strength equivalent to or more than that of a thick wall portion in a expanding process, the deformation of the thick wall portion is subsequently promoted, and as a result, a working coefficient is allowed to become uniform. On the other hand, it has been considered that, in single-phase steel, such as a Q/T material, having a high YR and a low work-hardening coefficient, the deformation of a thin wall portion preferentially occurs as a expanding process is performed, and hence the deformation reaches the limit of expand ratio at an early stage.

[0015] The present invention was made based on the above findings. That is, it was found that when Q/T treatment which is considered as a preferable process in conventional techniques is not intentionally used, and steel containing an alloying component (including equation) described in Claims is used which is in an as-rolled state or which is processed by a nonthermal-refining type heat treatment, the steel can be easily expanded although having a high strength, and that a high expand ratio can be realized; hence, the present invention was finally made. It is also considered that the properties described above can be obtained since the microstructure thus obtained contains ferrite and a low temperature-transforming phase.

[0016] That is, the present invention provides a seamless expandable oil country tubular goods in which 0.010% to less than 0.10% of C, 0.05% to 1% of Si, 0.5% to 4% of Mn, 0.03% or less of P, 0.015% or less of S, 0.01% to 0.06% of Al, 0.007% or less of N, and 0.005% or less of O are contained; at least one of Nb, Mo, and Cr is contained in the range of 0.01% to 0.2% of Nb, 0.05% to 0.5% of Mo, and 0.05% to 1.5% of Cr, so that the following equations (1) and (2) are satisfied; and Fe and unavoidable impurities are contained as the balance.

Note

$$\text{Mn} + 0.9 \times \text{Cr} + 2.6 \times \text{Mo} \geq 2.0 \quad (1)$$

$$4 \times \text{C} - 0.3 \times \text{Si} + \text{Mn} + 1.3 \times \text{Cr} + 1.5 \times \text{Mo} \leq 4.5 \quad (2)$$

In the above equations, the symbol of element represents the content (mass percent) of the element contained in steel.

[0017] In the present invention, instead of a part of the Fe mentioned above, at least one of 0.05% to 1% of Ni, 0.05% to 1% of Cu, 0.005% to 0.2% of V, 0.005% to 0.2% of Ti, 0.0005% to 0.0035% of B, and 0.001% to 0.005% of Ca may be contained.

[0018] In addition, in the present invention, instead of the equations (1) and (2), the following equations (3) and (4) may be satisfied.

Note

$$\text{Mn}+0.9\times\text{Cr}+2.6\times\text{Mo}+0.3\times\text{Ni}+0.3\times\text{Cu}\geq2.0 \quad (3)$$

$$4\times\text{C}-0.3\times\text{Si}+\text{Mn}+1.3\times\text{Cr}+1.5\times\text{Mo}+0.3\times\text{Ni}+0.6\times\text{Cu}\leq4.5 \quad (4)$$

In the above equations, the symbol of element represents the content (mass percent) of the element contained in steel.

[0019] In addition, in the present invention, the microstructure of a steel pipe preferably contains ferrite at a volume fraction of 5% to 70% and the balance substantially composed of a low temperature-transforming phase.

[0020] The term “substantially” implies that a third phase (other than ferrite and the low temperature-transforming phase) having a volute fraction of less than 5% is allowed to exist. As the third phase, for example, perlite, cementite, or retained austenite may be mentioned.

[0021] In addition, the present invention provides a method for manufacturing a seamless expandable oil country tubular goods, comprising the steps of: heating a raw material for a steel pipe, the raw material containing, on a mass percent basis, 0.010% to less than 0.10% of C, 0.05% to 1% of Si, 0.5% to 4% of Mn, 0.03% or less of P, 0.015% or less of S, 0.01 to 0.06% of Al, 0.007% or less of N, and 0.005% or less of O, at least one of 0.01% to 0.2% of Nb, 0.05% to 0.5% of Mo, and 0.05% to 1.5% of Cr, whenever necessary, at least one of 0.05% to 1% of Ni, 0.05% to 1% of Cu, 0.005% to 0.2% of V, 0.005% to 0.2% of Ti, 0.0005% to 0.0035% of B, and 0.001% to 0.005% of Ca, so that the above equations (3) and (4) are satisfied, and Fe and unavoidable impurities as the balance; forming a pipe by a seamless steel pipe-forming process (seamless pipe-forming process) which is performed at a rolling finish temperature of 800°C or

more; and whenever necessary, performing normalizing treatment after the pipe forming is performed by the seamless steel pipe-forming process.

[0022] In addition, the present invention provides a method for manufacturing a seamless expandable oil country tubular goods, comprising the steps of; after heating of the raw material for a steel pipe described above is performed, and pipe forming is performed by a seamless steel pipe-forming process, holding the pipe thus formed in a region of from point A₁ to point A₃, that is, in an (α/γ) dual-phase region, for five minutes or more as final heat treatment, and then performing air cooling.

Brief Description of the Drawings

[0023] Fig. 1 is a longitudinal cross-sectional view showing the structure used for a pipe-expansion test.

[0024] Figs. 2(a), 2(b), 2(c), and 2(d) are each a pattern showing an example of dual-phase heat treatment.

Reference numerals 1, 2, and 3 in Fig. 1 indicate a steel pipe, a plug, and a direction in which the plug is drawn out, respectively.

Best Mode for Carrying Out the Invention

[0025] First, the reasons the composition of steel is limited as described above will be described. The content of the component contained in the composition is represented by mass percent and is abbreviated as %.

C: 0.010% to less than 0.10%

[0026] In order to achieve the formation of a dual-phase microstructure containing ferrite and a low temperature-transforming phase by a general seamless pipe-forming process, low C-high Mn-Nb based steel or steel which contains at least one of an alloying element instead of high Mn and an element (Cr, Mo) instead of Nb must be used, in which the alloying element satisfies the equation (3) and the element (Cr, Mo) has an effect of delaying transformation similar to that of Nb. However, when C is 0.10% or more, perlite is liable to be formed, and on the other hand, when C is less than 0.010%, the strength becomes insufficient; hence, the content of C is set in the range of 0.010% to less than 0.10%.

Si: 0.05% to 1%

[0027] Si is added as a deoxidizing agent and contributes to the increase in strength; however, when the content is less than 0.05%, the effect cannot be obtained, and on the other hand, when the content is more than 1%, in addition to serious degradation in hot workability, the YR is increased, so that the pipe-expansion property is degraded. Hence, the content of Si is set in the range of 0.05% to 1%.

Mn: 0.5% to 4%

[0028] Mn is an important element for forming a low temperature-transforming phase. In the case in which a low C and an element having an effect of delaying transformation (Nb, Cr, Mo) form a composite, when Mn is an only element added to the composite, Mn at a content of 2% or more can achieve the formation of a dual-phase microstructure containing ferrite and a low-temperature-transforming phase, and when Mn is added together with another alloying element so that the equation (3) is satisfied, Mn at a content of 0.5% or more can achieve the formation described above. However, when the content is more than 4%, segregation may seriously occur,

and as a result, the toughness and the pipe-expansion property are degraded. Hence, the content of Mn is set in the range of 0.5% to 4%.

P: 0.03% or less

[0029] P is contained in steel as an impurity and is an element liable to cause grain boundary segregation; hence, when the content is more than 0.03%, the grain boundary strength is seriously decreased, and as a result, the toughness is decreased. Hence, the content of P is controlled to be 0.03% or less and is preferably set to 0.015% or less.

S: 0.015% or less

[0030] S is contained in steel as an impurity and is present primarily as an inclusion of an Mn-based sulfide. When the content is more than 0.015%, S is present as an extended large and coarse inclusion, and as a result, the toughness and the pipe-expansion property are seriously degraded. Hence, the content of S is controlled to be 0.015% or less and is preferably set to 0.006% or less. In addition, the structural control of the inclusion by Ca is also effective.

Al: 0.01% to 0.06%

[0031] Al is used as a deoxidizing agent; however, when the content is less than 0.01%, the effect is small, and when the content is more than 0.06%, in addition to the saturation of the effect, the amount of an alumina-based inclusion is increased, thereby degrading the toughness and the pipe-expansion property. Hence, the content of Al is set in the range of 0.01% to 0.06%.

N: 0.007% or less

[0032] N is contained in steel as an impurity and forms a nitride by bonding with an element such as Al or Ti. When the content is more than 0.007%, a large and coarse nitride is formed, and as a result, the toughness and the pipe-expansion property are degraded. Hence, the content of N is controlled to be 0.007% or less and is preferably set to 0.005% or less.

O: 0.005% or less

[0033] O is present in steel as an inclusion. When the content is more than 0.005%, the inclusion tends to be present in a coagulated form, and as a result, the toughness and the pipe-expansion property are degraded. Hence, the content of O is controlled to be 0.005% or less and is preferably set to 0.003% or less.

[0034] In addition to the elements described above, at least one of Nb, Mo, and Cr is added in the range described below.

Nb: 0.01% to 0.2%

[0035] Nb is an element suppressing the formation of perlite and contributes to the formation of a low temperature-transforming phase in a composite containing high C and high Mn. In addition, Nb contributes to the increase in strength by the formation of a carbonitride. However, when the content is less than 0.01%, the effect cannot be obtained, and on the other hand, when the content is more than 0.2%, in addition to the saturation of the effect described above, the formation of ferrite is also suppressed, so that the formation of a dual-phase microstructure containing ferrite and a low temperature-transforming phase is suppressed. Hence, the content of Nb is set in the range of 0.01% to 0.2%.

Mo: 0.05% to 0.5%

[0036] Mo forms a solid solution and carbide and has an effect of increasing strength at room temperature and at a high temperature; however, when the content is more than 0.5%, in addition to the saturation of the effect described above, the cost is increased, and hence Mo at a content of 0.5% or less may be added. In order to efficiently obtain the effect of increasing strength, the content is preferably set to 0.05% or more. In addition, as an element having an effect of delay-

ing transformation, Mo has an effect of suppressing the formation of perlite, and in order to efficiently obtain the effect described above, the content is preferably set to 0.05% or more.

Cr: 0.05% to 1.5%

[0037] Cr suppresses the formation of perlite, contributes to the formation of a dual-phase microstructure containing ferrite and a low temperature-transforming phase, and contributes to the increase in strength by hardening of the low temperature-transforming phase. However, when the content is less than 0.05%, the effect cannot be obtained. On the other hand, even when the content is increased to more than 1.5%, in addition to the saturation of the above effect, the formation of ferrite is also suppressed, and as a result, the formation of a dual-phase microstructure is suppressed. Hence, the content of Cr is set to 0.05% to 1.5%.

[0038] Under the conditions in which at least one of Nb, Mo, and Cr is contained and the content of a low C is less than 0.1%, in view of the suppression of the formation of perlite, the equation (3) must be satisfied, and in addition, in view of the promotion of the formation of ferrite at a volume fraction of 5% to 70%, the equation (4) must be satisfied.

[0039] In addition, in the case in which Ni and Cu are not added which will be described later, instead of the equation (3), the equation (1) is to be used, and instead of the equation (4), the equation (2) is to be used.

[0040] In addition to the elements described above, the following elements may also be added whenever necessary.

Ni: 0.05% to 1%

[0041] Ni is an effective element for improving strength, toughness, and corrosion resistance. In addition, when Cu is added, Cu cracking which may occur in rolling can be effectively prevented; however, since Ni is expensive, and the effect thereof is saturated even when the content

is excessively increased, the content is preferably set in the range of 0.05% to 1%. In particular, in view of Cu cracking, the content of Ni is preferably set so that the content (%) of $Cu \times 0.3$ or more is satisfied.

Cu: 0.05% to 1%

[0042] Cu is added in order to improve strength and corrosion resistance; however, in order to efficiently obtain the above effect, the content must be more than 0.05% or more, and on the other hand, when the content is more than 1%, since hot embrittlement is liable to occur, and the toughness is also decreased, the content is preferably set in the range of 0.05% to 1%.

V: 0.005% to 0.2%

[0043] V forms a carbonitride and has an effect of increasing strength by the formation of a microstructure having a finer microstructure and by the enhancement of precipitation; however, the effect is unclear at a content of less than 0.005%. In addition, when the content is more than 0.2%, since the effect is saturated, and problems of cracking in continuous casting and the like may arise, the content may be in the range of 0.005% to 0.2%.

Ti: 0.005% to 0.2%

[0044] Ti is an active element for forming a nitride, and by the addition of approximate N equivalents ($N\% \times 48/14$), N aging is suppressed. In addition, when the addition of B is performed, Ti may also be added so that the effect of B is not suppressed by precipitation and fixation thereof in the form of BN caused by N contained in steel. When Ti is further added, carbides having a microstructure are formed, and as a result, the strength is increased. The effect cannot be obtained at a content of less than 0.005%, and in particular, ($N\% \times 48/14$) or more is preferably added. On the other hand, when the content is more than 0.2%, since a large and

coarse nitride is liable to be formed, the toughness and the pipe-expansion property are degraded, and hence the content may be set to 0.2% or less.

B: 0.0005% to 0.0035%

[0045] B suppresses grain boundary cracking as an element for enhancing grain boundary and contributes to the improvement in toughness. In order to efficiently obtain the above effect, the content must be 0.0005% or more. On the other hand, even when the content is excessively increased, in addition to the saturation of the above effect, the ferrite transformation is suppressed, and hence the content is set to 0.0035% as an upper limit.

Ca: 0.001% to 0.005%

[0046] Ca is added so that an inclusion is formed into a spherical shape; however, in order to efficiently obtain the above effect, the content must be 0.001% or more, and when the content is more than 0.005%, since the effect is saturated, the content may be set in the range of 0.001% to 0.005%.

[0047] Next a preferable range of the composition of the present invention will be described.

[0048] In order to ensure a low YR and uniform elongation which are effective for the pipe-expansion property, the microstructure of a steel pipe is preferably a dual-phase microstructure which contains a substantially soft ferrite phase and a hard low temperature-transforming phase, and in order to ensure a TS of 600 MPa or more, the microstructure preferably contains ferrite at a volume fraction of 5% to 70% and the balance substantially composed of a low temperature-transforming phase. Since a significantly superior pipe-expansion property can be obtained, a ferrite volume fraction of 5% to 50% is more preferable, and in addition, a volume fraction of 5% to 30% is even more preferable. In addition, in the low temperature-transforming phase, bainitic ferrite (which is equivalent to acicular ferrite) is also contained as described above; how-

ever, unless the content of C is less than 0.02% in the composition of the present invention, this bainitic ferrite is hardly formed.

[0049] Next, a manufacturing method will be described.

[0050] Steel having the composition described above is preferably formed into a raw material for steel pipes such as billets by melting using a known melting method, such as a converter or an electric furnace, followed by casting using a known casting method such as a continuous casting method or an ingot-making method. Alternatively, after being formed by a continuous casting method or the like, a slab may be formed into a billet by rolling.

[0051] In addition, in order to decrease inclusions, measures to decrease inclusions, such as floatation treatment or coagulation suppression, are preferably taken when steel making and casting are performed. In addition, by forging in continuous casting or heat treatment in a soaking furnace, central segmentation may be decreased.

[0052] Next, after the raw material for steel pipes thus formed is heated, pipe forming by hot working is performed using a general Mannesmann-plug mill method, Mannesmann-mandrel mill method, or hot extrusion method, thereby forming a seamless steel pipe having desired dimensions. In this step, in view of a low YR and uniform elongation, final rolling is preferably finished at a temperature of 800°C or more so that a working strain is not allowed to remain. Cooling may be performed by general air cooling. In addition, in the range of the composition defined by the present invention, as long as unique low-temperature rolling in pipe forming or quenching thereafter is not performed, ferrite is formed, the balance is substantially composed of a low temperature-transforming phase, and the volume fraction of the ferrite is approximately in the range of 5% to 70%.

[0053] In addition, even in the case in which a predetermined microstructure is not obtained by an unusual pipe-forming step such as low-temperature rolling in pipe forming or quenching performed thereafter, when normalizing treatment is performed, a predetermined microstructure can be obtained. Furthermore, even when the rolling finish temperature is set to 800°C or more in pipe forming, non-uniform and anisotropic material properties may be generated depending on a manufacturing process in some cases, and in this case, normalizing treatment may also be performed whenever necessary. In the range of the composition according to the present invention, although a microstructure obtained after normalizing treatment is approximately equivalent to that of a microstructure obtained right after pipe forming, the non-uniform and anisotropic material properties generated in pipe forming are decreased, and as a result, a more superior pipe-expansion property can be obtained. Incidentally, in a temperature range of Ac_3 or more, the temperature of the normalizing treatment is preferably 1,000°C or less and is more preferably in the range of 950°C or less.

[0054] In addition, in order to realize a lower YR in the present invention, instead of the normalizing treatment, after the steel pipe is finally held in an (α/γ) dual-phase region, air cooling may be performed. In the range of the composition of the present invention, although a dual-phase microstructure containing ferrite and a low temperature-transforming phase is also obtained as is the case of the normalizing treatment, the strength of the ferrite is further decreased, and the decrease in YR is promoted. In order to obtain the effect described above, the holding time is required to be five minutes or more. In addition, since the effect described above does not depend on thermal hysteresis before the holding step performed in a dual-phase region, as shown in Fig. 2(a), 2(b), 2(c), and 2(d), heat treatment, such as heating to a γ region, followed

by cooling directly to an (α/γ) dual-phase region, or heating to a dual-phase region after quenching, may be performed in order to obtain an effect of grain refinement.

[0055] In this case, although point A_1 and point A_3 defining the (α/γ) dual-phase region are preferably measured accurately, the following equations may be conveniently used instead.

$$A_3 \text{ (}^{\circ}\text{C)} = 910 - 203 \times \sqrt{C} + 44.7 \times Si - 30 \times Mn - 15.2 \times Ni - 20 \times Cu - 11 \times Cr + 31.5 \times Mo + 104 \times V + 700 \times P + 400 \times Al + 400 \times Ti$$

$$A_1 \text{ (}^{\circ}\text{C)} = 723 + 29.1 \times Si - 10.7 \times Mn - 16.9 \times Ni + 16.9 \times Cr$$

In the above equations, the symbol of element represents the content (mass percent) of the element contained in steel.

EXAMPLE

[0056] After various types of steel having compositions shown in Table 1 were each cast into a steel ingot having a weight of 100 kg by vacuum melting, the ingots were then formed into billets by hot forging, followed by hot working for forming pipes using a model seamless rolling machine, thereby obtaining seamless steel pipes each having an external diameter of 4 inches (101.6 mm) and a wall thickness of 3/8 inches (9.525 mm). Rolling finish temperatures in this process are shown in Tables 2, 3, and 4.

[0057] Some of the steel pipes thus formed were processed by heat treatment, such as normalizing treatment, dual-phase heat treatment (Fig. 2(a), 2(b), 2(c), and 2(d)) or Q/T treatment. The normalizing treatment was performed by heating to a temperature of 890°C for 10 minutes, followed by air cooling. In the Q/T treatment, after heating was performed to 920°C for 60 minutes, water cooling was performed, and tempering treatment was performed at a temperature of 430 to 530°C for 30 minutes.

[0058] In this example, transformation points A_1 and A_3 of the dual-phase heat treatment were obtained by the following equations.

$$A_3 \text{ (}^{\circ}\text{C}\text{)} = 910 - 203 \times \sqrt{C} + 44.7 \times Si - 30 \times Mn - 15.2 \times Ni - 20 \times Cu - 11 \times Cr + 31.5 \times Mo + 104 \times V + 700 \times P + 400 \times Al + 400 \times Ti$$

$$A_1 \text{ (}^{\circ}\text{C}\text{)} = 723 + 29.1 \times Si - 10.7 \times Mn - 16.9 \times Ni + 16.9 \times Cr$$

In the above equations, the symbol of element represents the content (mass percent) of the element contained in steel.

[0059] For each steel pipe, the microstructure and the fraction of ferrite (volume fraction) were examined by observation using an optical microscope and a SEM (scanning electron microscope), and in addition, the tensile properties and the pipe-expansion property were also measured. The results are shown in Tables 2, 3, and 4. In this measurement, the tensile test was carried out in accordance with the tensile testing method defined by JIS Z2241, and as the test piece, JIS 12B was used which was defined in accordance with JIS Z2201. The pipe-expansion property was evaluated by an expand ratio (a limit of expand ratio) at which a pipe was expandable without causing any non-uniform deformation during pipe expansion, and in particular, an expand ratio at which the rate of wall-thickness deviation after pipe expansion did not exceed the rate of wall-thickness deviation before pipe expansion + 5% was used. The rate of wall-thickness deviation was obtained by measuring thicknesses at 16 points along the cross-section of the pipe at regular angular intervals of 22.5° using a ultrasonic thickness meter. For the pipe-expansion test, as shown in Fig. 1, a pressure-expansion method was performed in which plugs 2 having various maximum external diameters D_1 , each of which was larger than an internal diameter D_0 of a steel pipe 1 before expansion, were each inserted thereinto and then mechanically drawn out in a direction in which the plug was to be drawn out so that the inside diameter of the steel pipe is expanded, and the expansion ratio was obtained from the average internal diameters before and after the pipe expansion.

[0060] From Tables 2, 3, and 4, according to the present invention, it was found that a superior pipe-expansion property having a limit of expand ratio of 40% or more can be obtained.

Industrial Applicability

[0061] According to the present invention, even when the expand ratio is more than 30%, a steel pipe having a superior pipe-expansion property and a TS of 600 MPa or more can be supplied at an inexpensive price.

Table 1

Steel No.	C	Si	Mn	P	S	Al	N	O
A	0.048	0.54	3.36	0.015	0.003	0.032	0.0044	0.0018
B	0.081	0.21	3.05	0.011	0.001	0.040	0.0034	0.0021
C	0.025	0.20	2.85	0.008	0.001	0.027	0.0026	0.0022
D	0.051	0.19	2.20	0.012	0.005	0.041	0.0031	0.0029
E	0.047	0.30	3.30	0.010	0.002	0.035	0.0019	0.0008
F	0.040	0.21	3.88	0.012	0.001	0.032	0.0022	0.0020
G	0.008	0.25	3.22	0.013	0.003	0.038	0.0034	0.0018
H	0.16	0.36	3.10	0.014	0.001	0.040	0.0048	0.0032
I	0.056	0.19	1.58	0.015	0.004	0.039	0.0030	0.0029
J	0.25	0.21	1.45	0.012	0.002	0.030	0.0041	0.0037
K	0.045	0.29	3.04	0.009	0.001	0.023	0.0036	0.0020
L	0.081	0.24	2.21	0.010	0.002	0.018	0.0021	0.0009
M	0.047	0.64	1.65	0.011	0.001	0.040	0.0034	0.0028
N	0.032	0.35	2.70	0.016	0.003	0.041	0.0042	0.0019
O	0.087	0.21	2.56	0.015	0.003	0.022	0.0045	0.0033
P	0.092	0.34	2.21	0.018	0.005	0.032	0.0038	0.0020

 $P1 = Mn + 0.9 \times Cr + 2.6 \times Mo + 0.3 \times Ni + 0.3 \times Cu$ $P2 = 4 \times C - 0.3 \times Si + Mn + 1.3 \times Cr + 1.5 \times Mo + 0.3 \times Ni + 0.6 \times Cu$

In this table, the symbol of element represents the content (mass percent) of the element contained in steel.

Table 1 (Continued)

Steel No.	Nb	Cr	Mo	Ni	Cu	V	Ti	B	Ca	P1	P2	Remarks
A	0.044	-	-	-	-	-	-	-	-	3.63	3.66	Adequate
B	0.021	0.10	-	-	-	0.017	-	-	-	3.14	3.44	Adequate
C	0.022	0.11	0.20	0.88	-	0.015	0.0018	0.0021	3.73	3.60	Adequate	
D	0.024	0.82	-	-	0.045	0.021	0.0012	-	2.94	3.41	Adequate	
E	0.081	-	-	0.50	0.22	-	0.0025	0.0018	3.52	3.68	Adequate	
F	0.019	-	0.31	-	0.022	-	-	-	4.69	4.44	Adequate	
G	0.045	0.20	-	0.20	0.22	-	0.014	0.0030	0.0022	3.53	3.63	Inadequate
H	0.021	-	-	-	0.021	0.021	-	-	3.10	3.63	Inadequate	
I	0.035	-	-	0.21	0.19	0.055	0.014	0.0012	-	1.70	1.92	Inadequate
J	-	1.12	0.72	-	-	0.17	0.009	-	-	4.33	4.92	Inadequate
K	-	0.41	-	-	-	-	-	-	-	3.41	3.67	Adequate
L	-	-	0.25	-	-	-	-	-	-	2.86	2.84	Adequate
M	-	1.23	0.13	0.20	-	-	0.015	-	-	3.16	3.50	Adequate
N	0.034	-	0.20	-	0.035	0.012	-	0.0020	3.22	3.02	Adequate	
O	-	1.23	0.13	0.32	0.45	-	0.0016	0.0021	4.24	5.01	Inadequate	
P	-	-	-	-	0.028	0.008	-	-	2.21	2.48	Inadequate	

Table 2

Steel pipe no.	Rolling temperature /°C	Finish Heat treatment	Substantial microstructure	α Fraction/volume %	Tensile properties			Rate of wall-thickness deviation before pipe expansion /%	Rate of wall-thickness deviation after pipe expansion /%	Limit of expand ratio /%	Remarks	
					YS /MPa	TS /MPa	YR /%					
1 A	820	-	α + Low temperature-transforming phase	18	483	662	73	15	34	4.2	9.0	43 Example
2 A	820	Normalizing treatment	α + Low temperature-transforming phase	20	464	653	71	16	35	3.9	8.4	45 Example
3 B	815	-	α + Low temperature-transforming phase	11	596	852	70	14	32	2.8	7.7	50 Example
4 B	815	Normalizing treatment	α + Low temperature-transforming phase	12	574	844	68	15	34	2.9	7.5	53 Example
5 B	730	Normalizing treatment	α + Low temperature-transforming phase	14	591	857	69	16	33	2.1	7.0	50 Example
5' B	820	Dual-phase region I	α + Low temperature-transforming phase	31	454	782	58	19	38	3.2	8.2	53 Example
6 C	855	-	α + Low temperature-transforming phase	9	456	634	72	18	40	6.7	11.5	48 Example
7 C	750	Normalizing treatment	α + Low temperature-transforming phase	11	468	641	73	17	39	6.0	10.8	46 Example
8 D	845	-	α + Low temperature-transforming phase	22	519	821	72	15	37	4.0	8.8	50 Example
9 D	730	Normalizing treatment	α + Low temperature-transforming phase	17	543	734	74	15	36	7.7	12.3	50 Example
10 E	860	-	α + Low temperature-transforming phase	15	564	842	67	16	34	4.2	9.0	55 Example

α : Ferrite, YS: Yield Strength, TS: Tensile Strength, YR: Yield Ratio, u-EI: Uniform Elongation, EI: Elongation

Table 3

Steel pipe no.	Steel no.	Rolling finish temperature /°C	Heat treatment	Substantial microstructure	α Fraction/volume %	Tensile properties				Rate of wall-thickness deviation after pipe expansion /%	Limit of expand ratio /%	Remarks
						YS /MPa	TS /MPa	YR /%	$u \cdot E$ /%			
11	E	860	Normalizing treatment	α + Low temperature-transforming phase	17	542	834	65	16	36	4.2	9.2
11'	E	860	Dual-phase region II	α + Low temperature-transforming phase	34	452	780	58	19	38	3.7	8.7
12	F	900	-	α + Low temperature-transforming phase	9	666	952	70	13	29	2.8	7.8
13	F	760	Normalizing treatment	α + Low temperature-transforming phase	10	649	940	69	14	30	3.8	8.4
14	G	840	-	Low temperature-transforming phase	-	470	546	86	10	31	7.2	12.0
15	H	825	-	α + Perlite + low temperature-transforming phase	37	514	650	79	12	35	3.8	8.5
16	H	740	-	α + Perlite + low temperature-transforming phase	51	571	705	81	11	31	5.5	10.0
17	I	825	-	α + Perlite + low temperature-transforming phase	32	434	543	80	16	40	7.1	12.0
18	I	825	Q/T Treatment	Tempered martensite	-	626	688	91	9	34	7.1	11.8
19	J	830	-	α + Perlite	62	504	586	86	14	39	4.4	9.0
20	J	830	Q/T Treatment	Tempered martensite	-	599	642	93	7	32	4.4	9.2

a: Ferrite, YS: Yield Strength, TS: Tensile Strength, YR: Yield Ratio, $u \cdot E$: Uniform Elongation, El: Elongation

Table 4

Steel Pipe no.	Steel no.	Rolling finish temperature /°C	Heat treatment	Substantial microstructure	α Fraction/volume %	Tensile properties				Rate of wall-thickness deviation before pipe expansion /%	Rate of wall-thickness deviation after pipe expansion /%	Limit of expand ratio /%	Remarks	
						YS / MPa	TS / MPa	YR /%	u-EI /%					
21	K	830	-	α + Low temperature-transforming phase	38	456	702	65	17	38	3.8	8.8	48	Example
22	K	750	Normalizing treatment	α + Low temperature-transforming phase	36	462	689	67	18	39	4.2	9.1	50	Example
23	K	830	Dual-phase region IV	α + Low temperature-transforming phase	48	360	631	57	20	42	3.8	8.8	55	Example
24	L	825	-	α + Low temperature-transforming phase	36	439	708	62	17	37	3.0	7.9	50	Example
25	L	760	Dual-phase region II	α + Low temperature-transforming phase	42	373	678	55	19	39	2.1	7.1	53	Example
26	M	815	-	α + Low temperature-transforming phase	19	624	892	70	14	31	6.4	11.3	45	Example
27	M	800	Normalizing treatment	α + Low temperature-transforming phase	21	577	888	65	15	32	5.7	10.6	48	Example
28	N	820	-	α + Low temperature-transforming phase	42	450	693	65	19	39	3.8	8.7	53	Example
29	N	730	Normalizing treatment	α + Low temperature-transforming phase	40	458	684	67	18	38	4.2	9.1	55	Example
30	N	830	Dual-phase region IV	α + Low temperature-transforming phase	49	386	655	59	20	41	2.7	7.7	57	Example
31	Ω	830	-	Low temperature-transforming phase	-	791	933	83	7	21	3.1	8.0	28	Comparative example
32	P	820	-	α + Perlite + low temperature-transforming phase	46	523	654	80	15	34	5.4	10.4	30	Comparative Example
33	P	730	Normalizing treatment	α + Perlite + low temperature-transforming phase	41	503	637	79	16	35	5.4	10.3	33	Comparative Example

α: Ferrite, YS: Yield Strength, TS: Tensile Strength, YR: Uniform Elongation, u-EI: Elongation